A Bidirectional Power Converter for AC Grid and DC Bus

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Abstract

Abstract This paper presents the development of a bidirectional converter for AC grid and DC bus. The converter adopts a full-bridge structure and utilizes average current control and sine pulse width modulation techniques for power factor correction and inverter design. The system's control core is based on a control chip, combined with control technology. By sensitis the input and output voltages, the pulse mdulation period is aclaulated to enhance the compensation speed of the overall control loop. This enables the converter to exhibit high power factor and stable output voltage capabilities, while anximum rated output of 1 kW experimental platform was constructed to emalate AC grid of 220 V and a DC bus of 400 V, thereby validating the theoretical analysis and design methods proposed in this paper. The experimental results showed that with an AC grid voltage of 220 V, the efficiency reached a maximum rated analysis and the efficiency reached a maximum of 96.98%. Through the converter, energy was fed back to the AC grid, achieving the objective of bidirectional energy scheduling. 1 Introduction

Introduction

Introduction As the seles of DC appliances and electric vehicles continue to climb year by year, it will lead to a gradual increase in electricity demand. If proper energy management is not implemented in the future, it may result in an inadjuate power supply, potentially impacting the operation of the AC electricity of a selectric and the selectric



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Figure 1 Bidirectional Converters Reveen AC Grid and DC Bus
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Literature [3]-[6] introduces bidirectional ACDC converters, all of which adopt a forcertion circuit, combined with a rear-stage IID-bidge resonant DC-to-DC converter achieving the functionality of high-voltage boosting and bucking for bidirectional ACDC converter or approximation of the structure structure converter in (3). Internough parallel connection, it effectively reduces current structure provides bidirectional ACDC converter or components, complex feedback control (3). FOCC converter or outper or components, complex feedback control (3). FOCC converter or outper technical provides bidirectional ACDC converter or outper technical provides bidirectional ACDC converter or components, complex feedback control (3). FOCC converter or outper technical provides bidirectional ACDC converter or outper technical provides bidirectional ACDC converter or controls DC-to-DC converter or and the structure is structure is structure is structure bidirection and DC-to-AC using sinusoidal pulse width modulation. This structure bises of ACDC converter or nulls is suitable for higher-power applications, trains studied the for high-eropower applications, structure and the train stage also requires control of multiple switching components and the constructure is straightforward and can handle a wide range of input prover architecture is straightforward and can handle a wide range of input site activations, it is suitable for higher-power applications, the insultable only for lower-straightforward and can handle a wide range of input site activations, it is suitable for higher-power applications, the insultable only for lower-straightforward and can handle a wide range of input site activation and the straightforward and can handle a wide range of input site activations, it is suitable for higher-power applications, it is suitable for higher-power applications, it is suitable for higher-power

Circuit Architecture and Controller Design

2.1 Circuit Architecture

2.1 Circuit Architecture Figure 2: illustrates the complete architecture of the bidirectional converter between the AC grid and the DC bus proposed in this paper. The hardware circuit primarily consists of (1) power factor correction inductors, (2) output voltage sensors, (7) ourrent sensors, and (8) a microcontroller controller, providing bidirectional energy transfer between the AC grid and the DC bus, in the forward mode, it should provide stable DC output voltage, lower total harmonic distortion, improved power factor, and higher conversion efficiency. In the reverse mode, it should be capable of feeding excess energy from the DC bus back to the AC grid autorate and output a voltage that is synchronized with the frequency and phase of the AC grid.



2.2 Feedback Control Method

In order to achieve advantages such as higher rated power, higher conversion efficiency, and a smaller circuit volume for the converter in this paper, the average current control method in continuous conduction mode will be used as the design foundation. Figure 3 illustrates the feedback block diagram of the average current control method.



Figure 3 Feedback Block Diagram of Average Current Control Method Figure 3 recutack Book Digating of Average Lintent Control Network The control method operates at a fixed frequency and, after comparing the output voltage with a reference value, the resulting error signal is multiplied by a multiplier to generate an average current reference signal. This reference signal is then used in conjunction with the inductor current for current loop compensation. After comparing it with a triangular/saw tooth carrier signal, a duty cycle signal is obtained, which changes with variations in the input voltage, to control the energy on the inductor, ensuring that the inductor current tracks the average current, as shown in Figure 4.



2.3 Sine Wave Pulse Width Modulation Design

2.3 Sine Wave Pulse Width Modulation (DSYM) is a modulation technique based on pulse width modulation (SYMV) is a modulation technique based on pulse width modulation. It involves comparing a sine wave signal with a triangulat carrier or save tooth carrier signal. As a result, the duty cycle of the pulses is determined by the sine wave. When the sine wave has a higher duty cycle, and conversely, when the sine wave has a lower magnitude, the duty cycle determined harmonic components in the current, effectively reducing total harmonic distortion. Therefore, the bipolar sinusoidal pulse width modulation is chosen as the switching signal modulation method for the bidirectional converter. Figure 5 shows the switching state waveform.



This paper designs and simulates a 1 kW bidirectional converter between the AC grid and the DC bus, taking into account relevant specifications for the AC grid system and the DC bus, as well as market demands for electricity consumption in AC grid and DC bus systems. The circuit specifications are shown in Table 1

Table 1 Electrical Specifications of the Converter	
Parameters	Specifications
Rated Voltage at the AC Grid Side	AC 220 V
Rated Current at the AC Grid Side	AC 5 A
Power Frequency at the AC Grid Side	60 Hz
Rated Voltage at the DC Bus	DC 400 V
Rated Maximum Conversion Power	1000 W
Circuit Switching Frequency	80 kHz

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Table 2 presents the selected actual circuit component parameters for this converter. In order to improve the efficiency of the converter, this paper uses new wide-bandgap witches instead of traditional silicon switches. These switches have lower switching losses at high frequencies, which can enhance the circuit's conversion efficiency.

Table 2 Selection of Circuit Component Parameters		
Component Parameter	Values	
Power Factor Correction Inductor	473.5μH 1299μF	
DC-Side Filtering Capacitor	0.68µF	
Thermistor	20Ω	
Barren Carritale	UE3C065080K4S (SiC)	

3.1 Steady-State Implementation Waveforms in Forward Mode

The practical circuit waveforms of AC voltage, current, DC voltage, and current under different loads with an AC voltage of 220 V are shown in Figure 6. The waveforms demonstrate that the circuit operates in the forward energy storage mode, and it achieves power factor correction under different loads.



 $\begin{array}{l} P_{BC_{c}Grid}: 5kW/div \; v_{DC_{c}Bus}: 500V/div\\ ip_{C_{c}Bus}: 2A/div \; P_{DC_{c}Bus}: 2kW/div time: 10ms/div\\ V_{AC_{c}Grid}= 220V \; , V_{DC_{c}Bus}= 400V \; , i_{DC_{c}Bus}= 2.5A \end{array}$ Figure 6 Experimental Waveforms in Forward Mode at 220 V

3.2 Steady-State Implementation Waveforms in Inverter Mode

Figure 7 displays the practical circuit waveforms during 1 kW grid feedback in the inverter mode. The waveforms illustrate that the converter maintains stable operation in the inverter mode and can feed back power to the AC grid port at different power levels. To verify maximum power feedback to the grid, this paper uses a fixed inductor current probe measurement direction and implements inversion at VAC Grid =220 V



 v_{AC_Grid} : 500V/div i_L : 10A/div PAC_Grid: 5kW/div vDC_Bas : 500V/div i_{DC_Bus} ; 2A/div P_{DC_Bus} ; 2kW/div time : 10ms/div V_{AC_Grid} = 220V · V_{DC_Bus} = 400V · P_{DC_Bus} = 1000W Figure 7 Experimental Waveforms in Inverter Mode at 220 V

3.3 Experimental Data for the Bidirectional Converter

5.5 Experimental Data for the Biddrectional Converter Figure 8 shows the efficiency curve of the converter operating in forward mode, with the AC grid $V_{AC,Gul}$ fixed at 220 V and the DC bus $V_{AC,Gul}$ fixed at 400 V, while varying the DC bus load current from light load to full load. From the curve, it can be observed that efficiency improves with increasing watage, with the highest conversion efficiency being 97.07% near full load at 220 V.





Figure 9 illustrates the efficiency curve in Forward Mode at 220 V Figure 9 illustrates the efficiency curve of the converter operating in the inverter mode at 220 V. The AC grid port $V_{C,Code}$ if Street at 220 V, and the DC bus $V_{D,C,Ret}$ is set at 400 V, while varying the feedback power from the DC bus to the grid, ranging from light load to full load. From the curve, it can be observed that efficiency improves with increasing wattace, with the highest conversion efficiency being 96.98% near full load at 220 V.



Through actual circuit measurements, power factor (PF) curves and total harmonic (THD) curves for the bidirectional converter operating in forward and inverter n be obtained, as shown in Figures 10 and 11. It can be observed that except for light loads, the PF values are all above 0.9, and the THD values are all below ion (THD) curves for the bidirectional conv dis modes can h



Figure 10 Po ver Factor (PF) Curve of the Bidirectional Converter Between AC Grid and DC Bus



Figure 11 Total Harmonic Distortion (THD) Curve of the Bidirectional Converter Between AC Grid and DC Bus

Conclusion

4 Conclusion This paper presents a bidirectional converter between the AC grid and the DC bus, designed and realized using digital signal processing. The converter achieves a rated power of 1 kW for both the AC grid and the DC bus. The circuit architecture primarily consists of a full-bridge converter, and the system utilizes average current control and sinusoidal pulse width modulation (SPWM) techniques for bidirectional energy transfer control. To enhance the stability and reliability of the system, this paper combines control techniques. It employs digital signal sensing of input and output voltages and calculates pulse width modulation periods, addressing the issue of slow compensation in traditional power factor and stable output voltage. Additionally, in inverter mode, it functions as an inverter to achieve bidirectional energy transfer.